Inventor: HUI et al.
Docket: 12364.27USU1
Title: MUM POWER TRACKING TECHNIQUE FOR SOLAR PANE
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Phon No.: 612.336.4638
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$0 < t < d_1 T_S$

$d_1 T_S < t < d T_S$

$d T_S < t < T_S$

(a)

(b)

Fig. 3 Operating principle. (a) Topology sequence. (b) Theoretical waveforms of v_C and v_D.

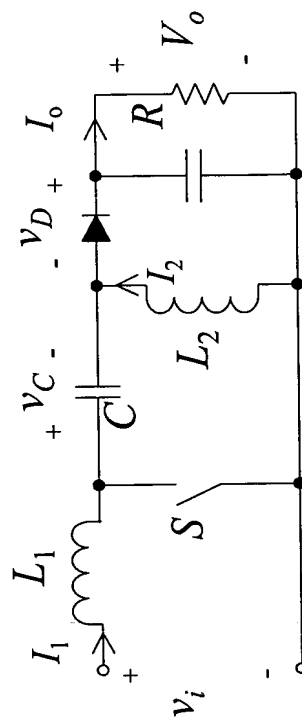Fig. 1 Equivalent circuit of a solar panel connecting to a converter.
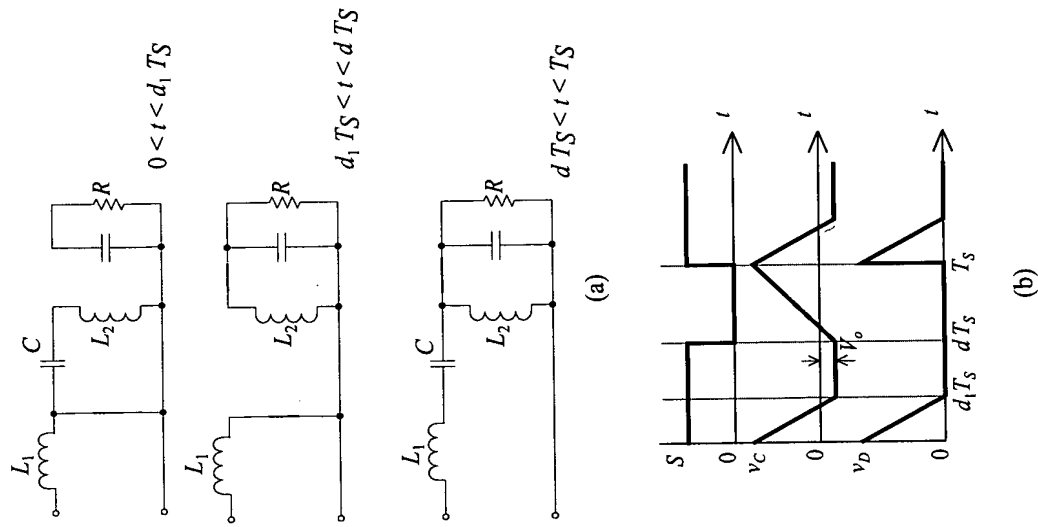
Fig. 2 SEPIC converter circuit.

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(a)

(b)

Fig. 6 Solar panel characteristics at different P_{lamp}. (a) i_g versus v_g. (b) P_O versus r_i.
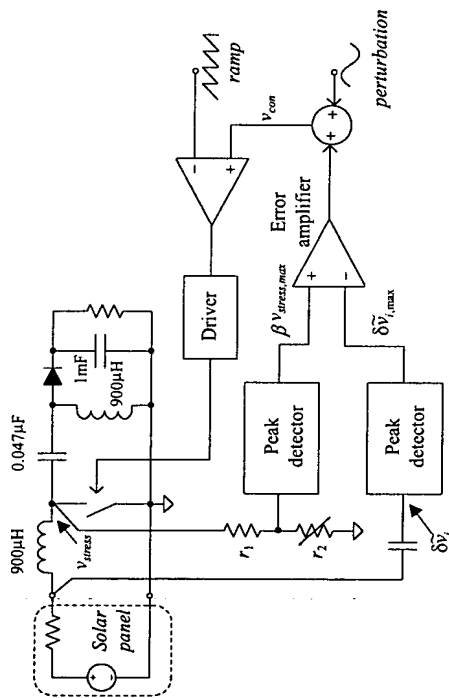

Fig. 4 Block diagram of proposed MPP tracking method.
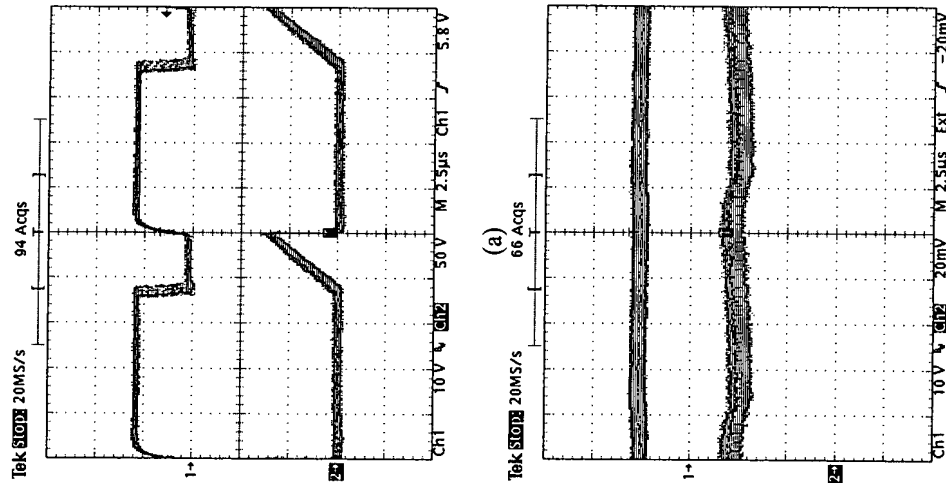

Fig. 5 Experimental setup for the solar panel.

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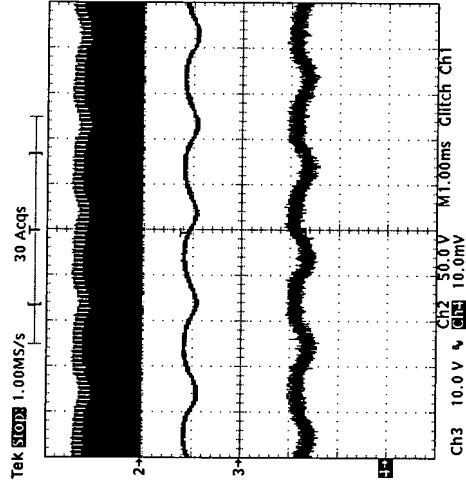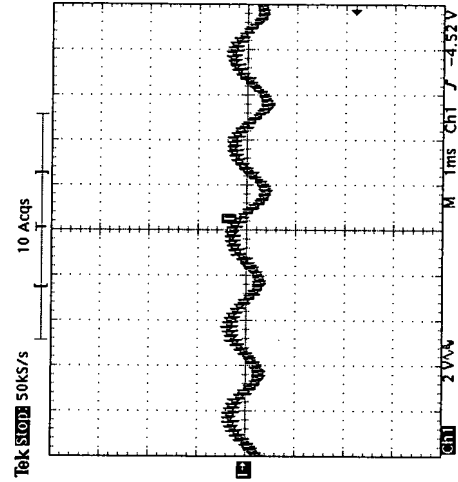Phone No.: 612.336.4638
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Fig. 8 Experimental waveforms of the SEPIC converter. Ch2: switch voltage stress, 50V/div; Ch3: input voltage, 10V/div; Ch4: input current, 0.5A/div.
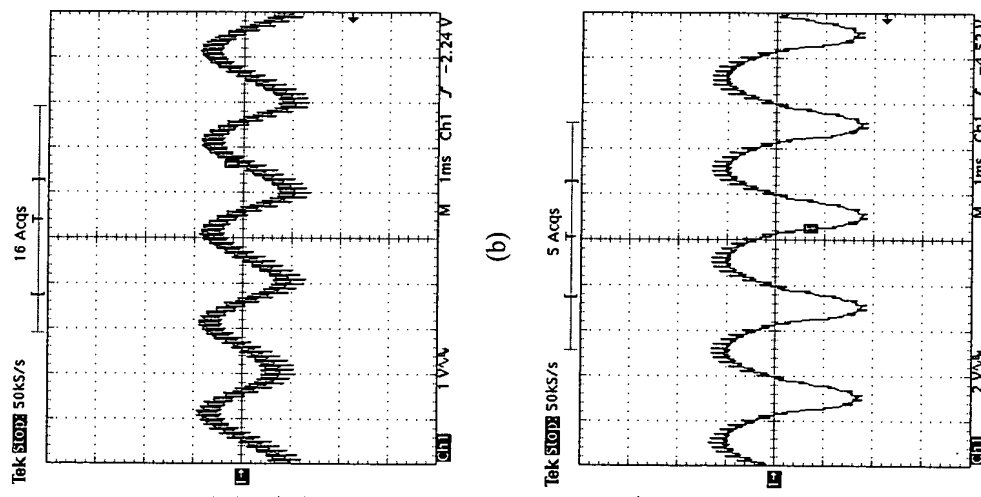
(a)

Fig. 7 Detailed experimental waveforms of the SEPIC converter. (a) Ch1: gate signal, 10V/div; Ch2: switch voltage stress, 50V/div. (b) Ch1: input voltage, 10V/div; Ch2: input current, 0.5A/div.

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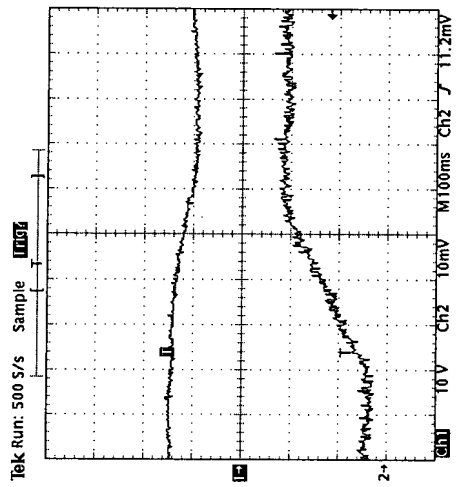Phone No.: 612.336.4638
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Fig. 10 Transient waveforms of the SEPIC converter subject to P_{lamp} changed from 500W to 900W. Ch1: input voltage, 10V/div. Ch2: input current, 0.5A/div.
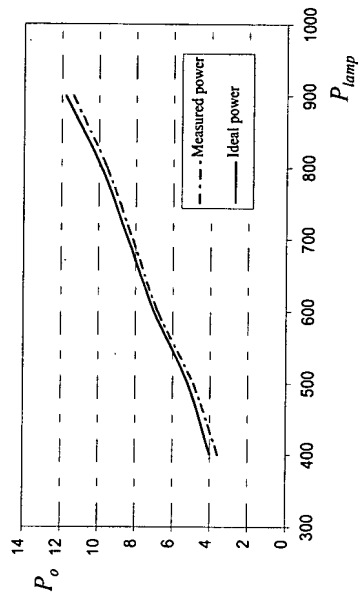

Fig. 11 Comparison of maximum solar panel output power using proposed method and the ideal ones in Fig. 6(b), under different P_{lamp}.

(b)

(c)

Fig. 9 Waveform of $\delta\tilde{v}_i$ with respect to different value of $\Re$. (a) $\Re = 0.02$. (b) $\Re = 0.05$. (c) $\Re = 0.1$.

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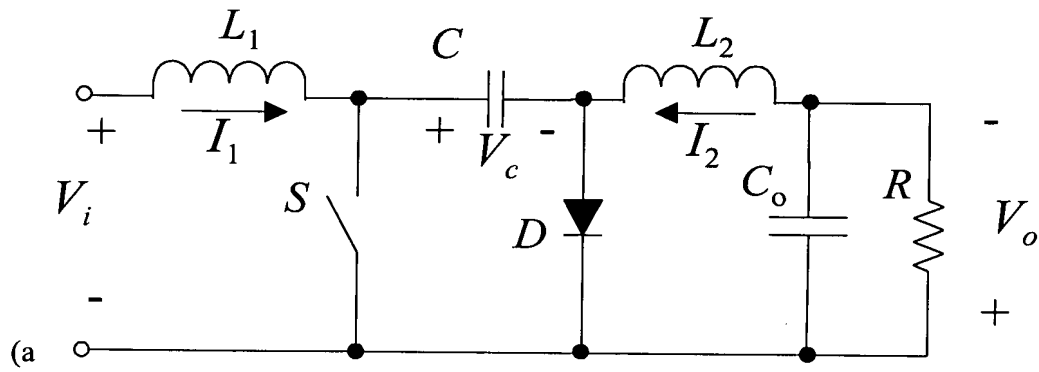
Fig. 12 Circuit diagram of the Cuk converter.

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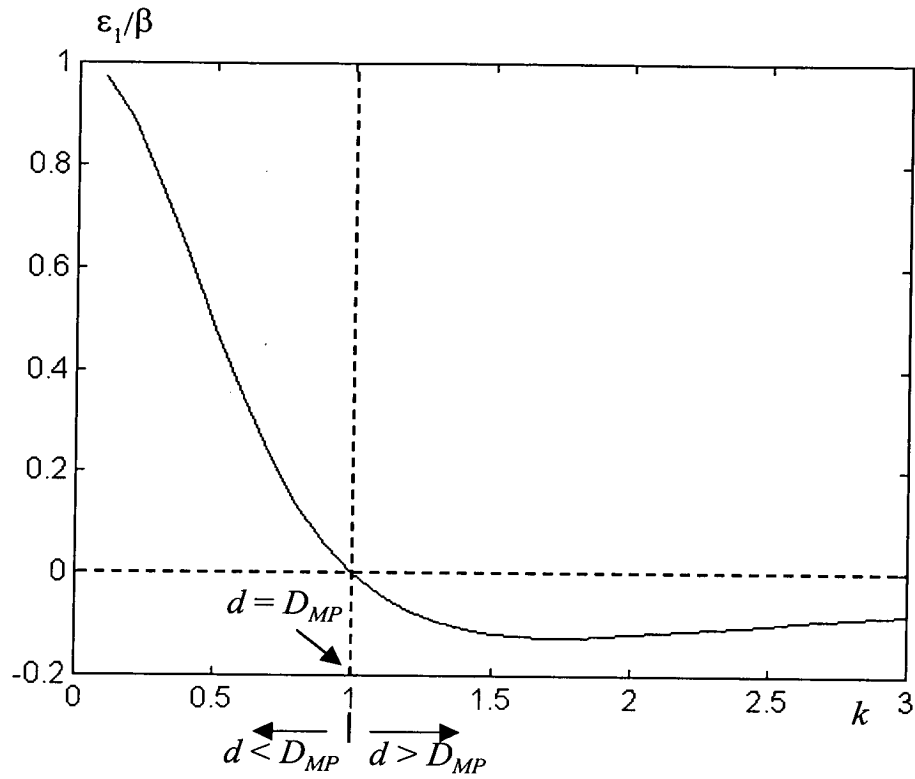
Fig. 13 Relationships between ε_1 / β and k.

Fig. 14 The proposed MPP tracking method.

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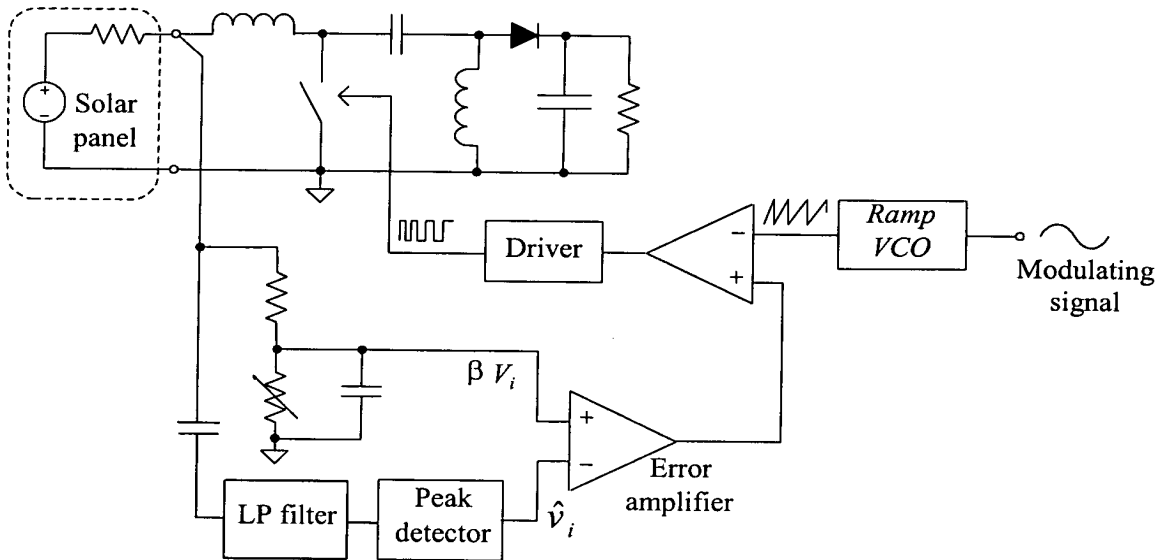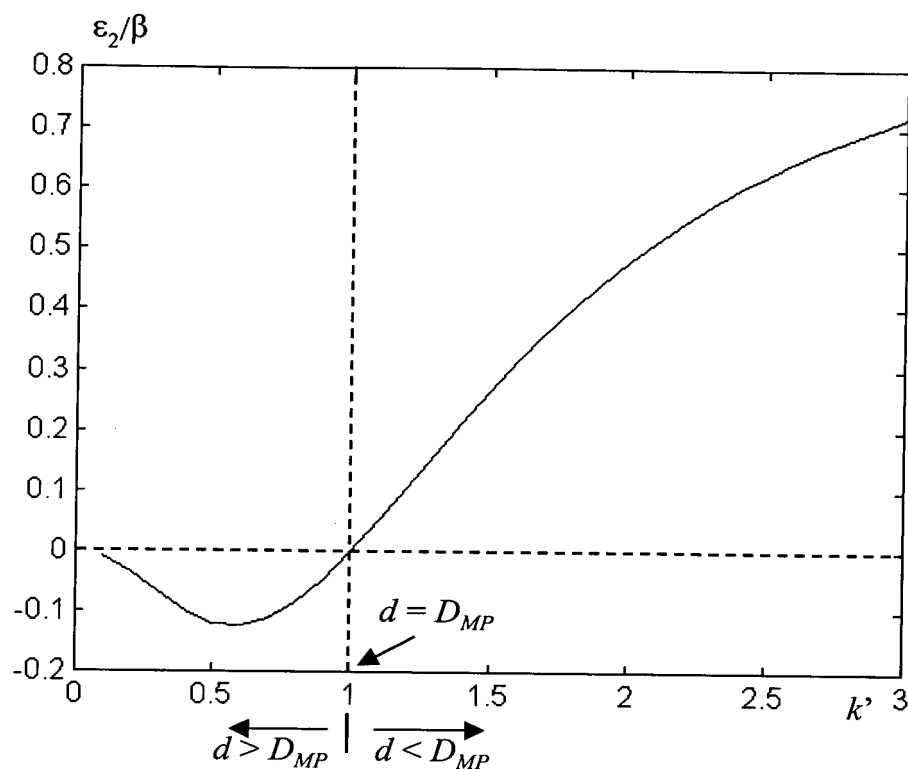
Fig. 15 Relationships between ε_2 / β and k*'.*
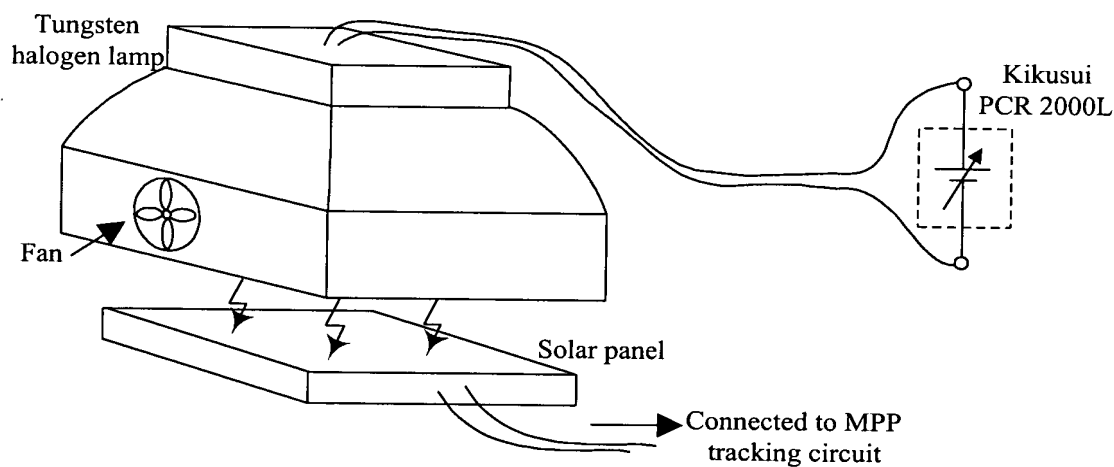

Fig. 16 Experimental setup for studying the proposed MPP tracking technique.

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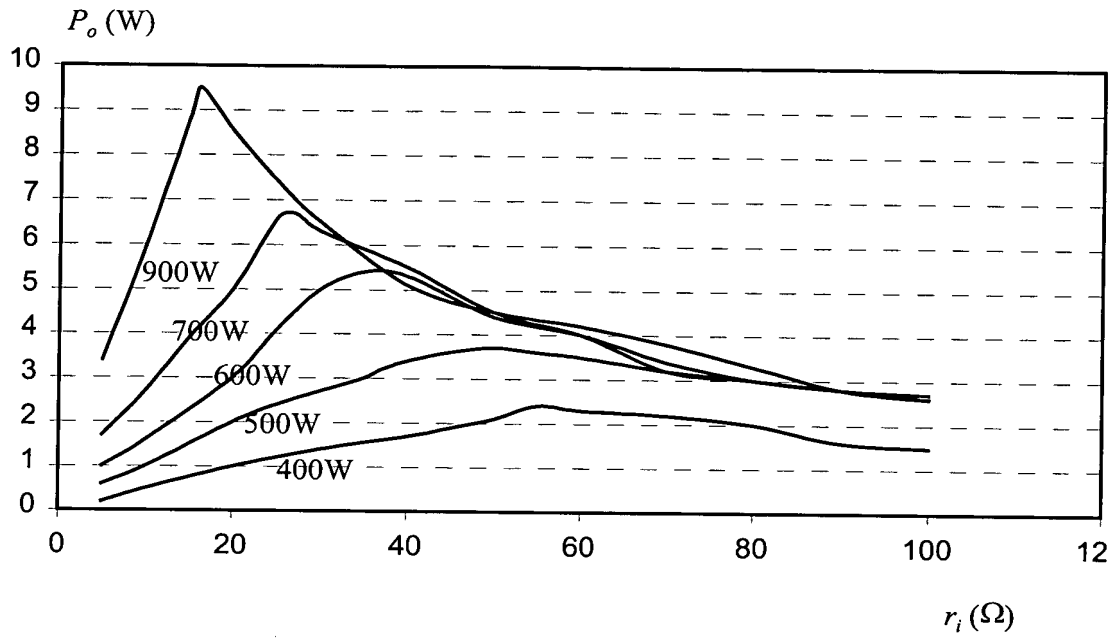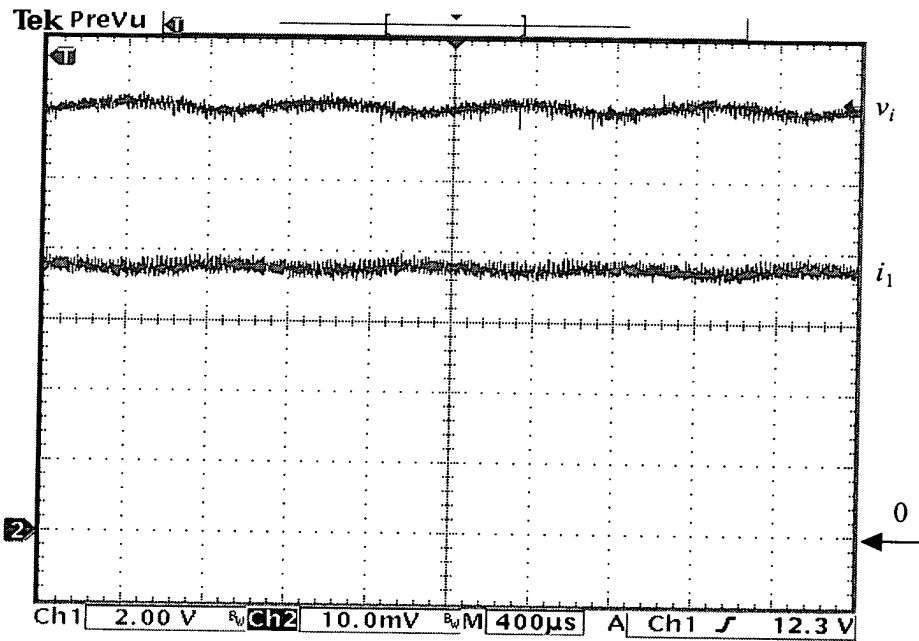Attorney Name: Michael D. Schumann (Reg. No. 30,422)
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Fig. 17. $P_o - r_i$ characteristics of the solar panel at different P_{lamp}.

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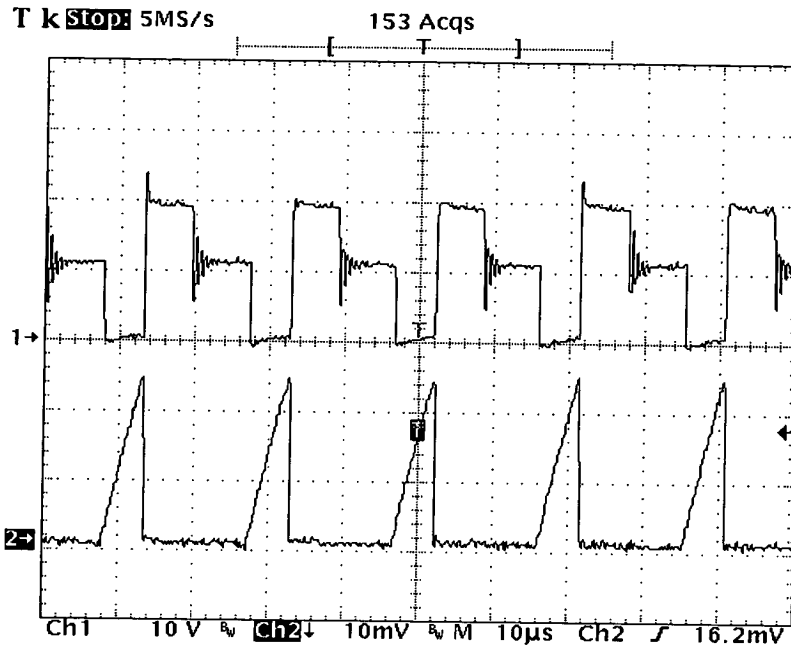Phone No.: 612.336.4638
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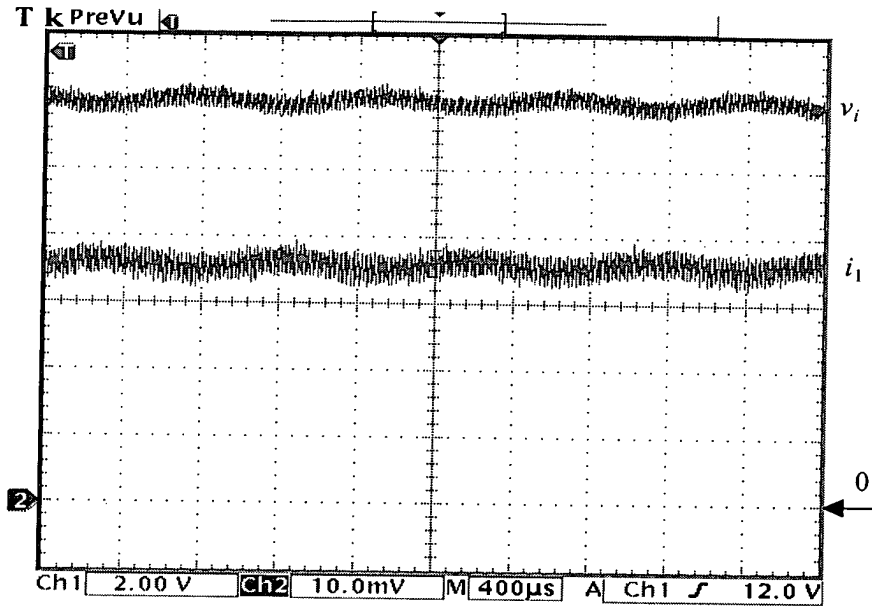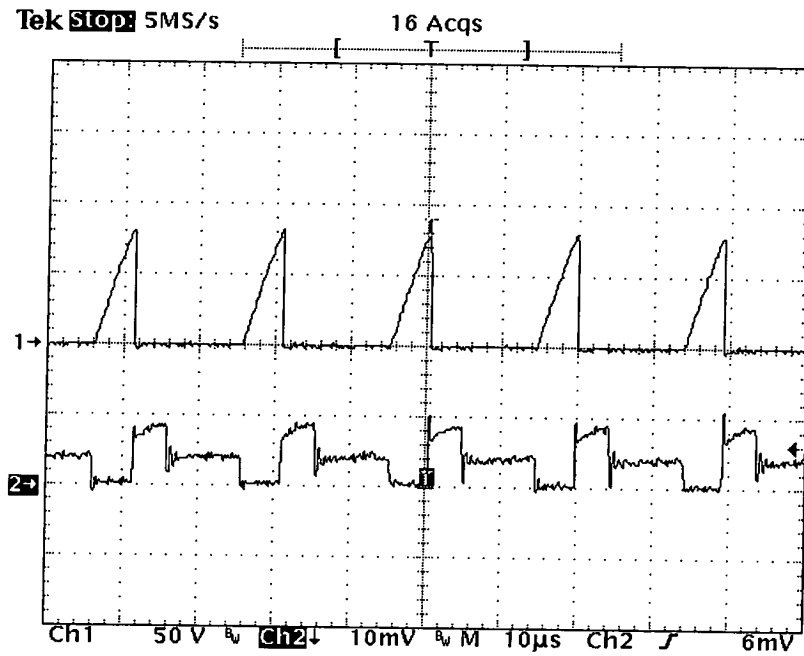
(a) DICM. (v_i: 2V/div. i_1: 0.2A/div.)

(b) DCVM. (v_i: 2V/div. i_1: 0.2A/div.)

Fig.18. Experimental waveforms of v_i and i_1 of the two SEPIC prototypes at the MPP when P_{lamp} equals 900W.

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T k Stop 5MS/s   153 Acqs

Ch1   10 V   Ch2↓   10mV   M   10µs   Ch2   ƒ   16.2mV

(a) Voltage and current stress on S in DICM. (Ch1: 10V/div. Ch2: 2A/div.)

Tek Stop 5MS/s   16 Acqs

Ch1   50 V   Ch2↓   10mV   M   10µs   Ch2   ƒ   6mV

(a) Voltage and current stress on S in DCVM. (Ch1: 50V/div. Ch2: 2A/div.)

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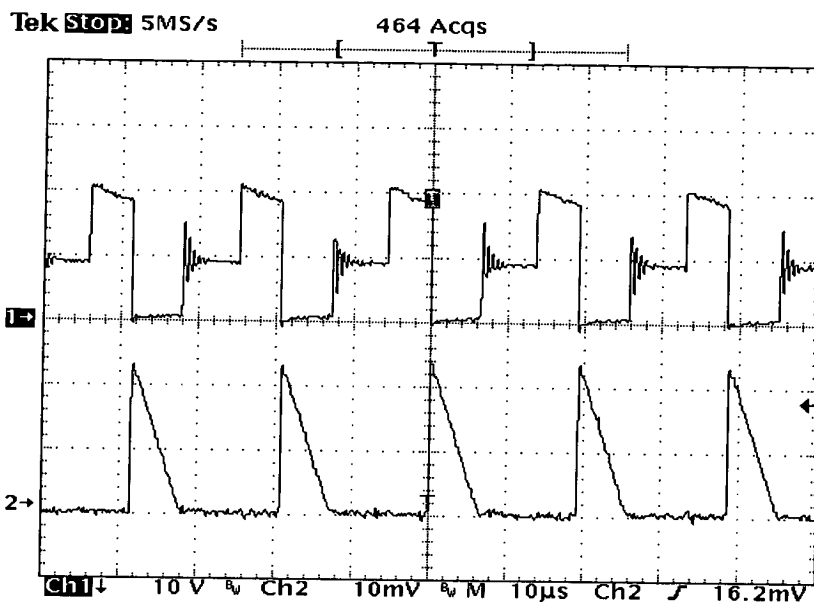Phone No.: 612.336.4638
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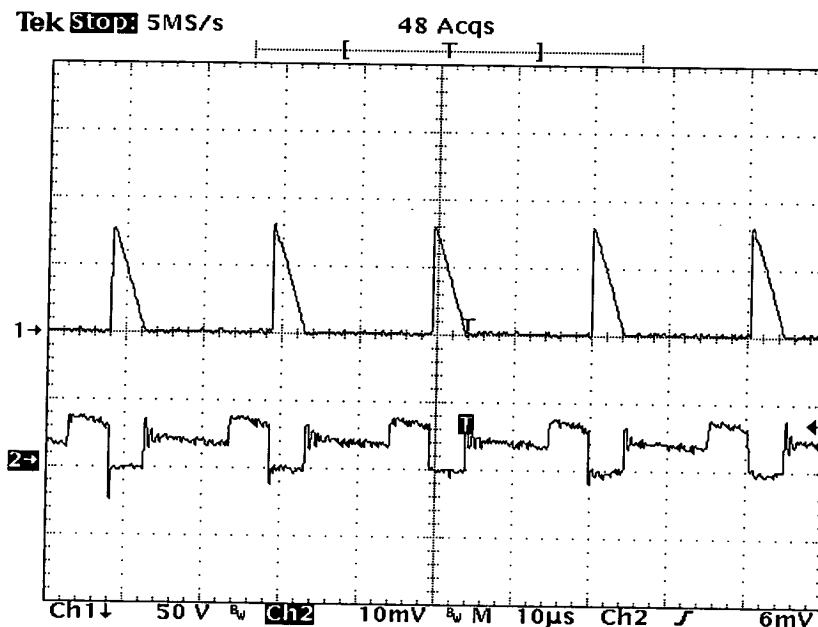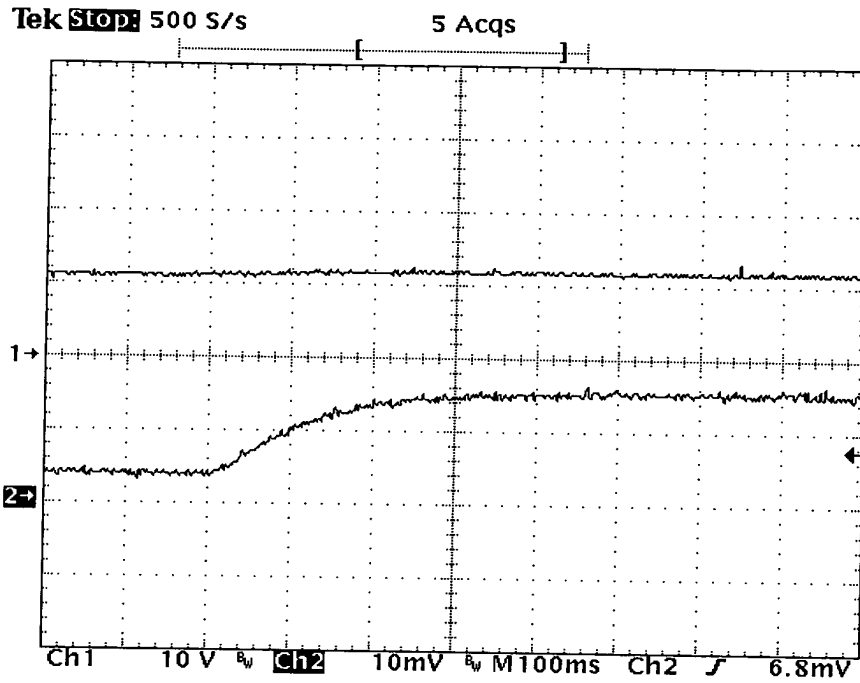
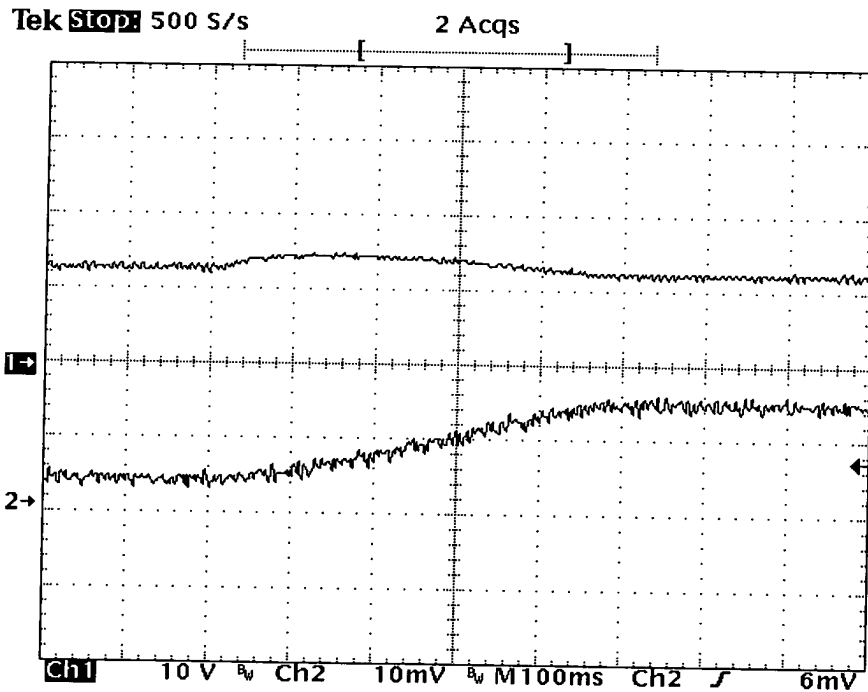(c) Voltage and current stress on D in DICM. (Ch1: 10V/div. Ch2: 2A/div.)

(d) Voltage and current stress on D in DCVM. (Ch1: 50V/div. Ch2: 2A/div.)

Fig.19. Experimental voltage and current stresses on S and D. (Timebase: 10µs/div)
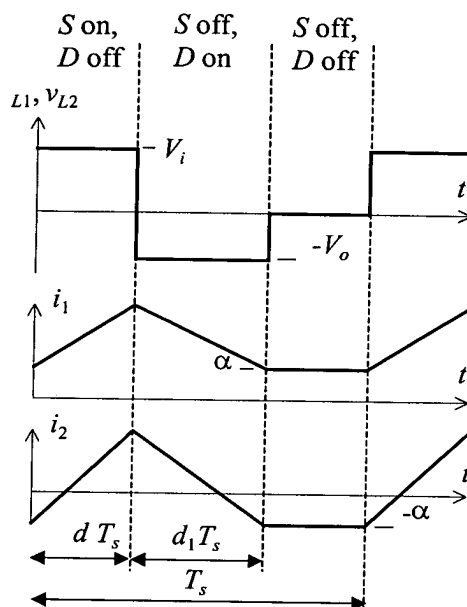
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Tek **Stop** 500 S/s   5 Acqs
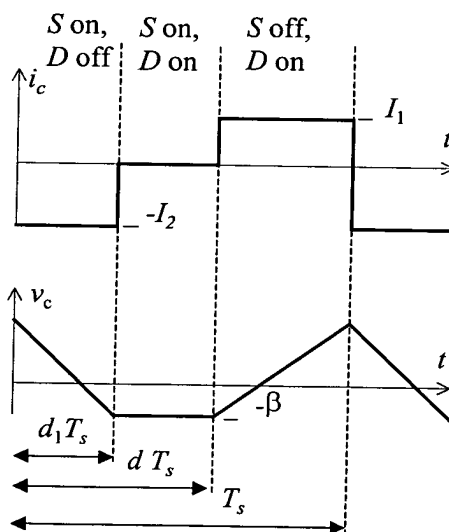
(a) DICM.

Tek **Stop** 500 S/s   2 Acqs

(b) DCVM.

Fig. 20. Experimental waveforms of the SEPIC converters when P_{lamp} is subject to a change from 400W to 900W. (Ch1: V_i, 10V/div. Ch2: I_1, 0.5A/div.)

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(a) Voltage and current waveforms of L_1 and L_2 in DICM.

(b) Current and voltage waveforms of C in DCVM.

Fig. 21 Key waveforms of SEPIC and Cuk converter.